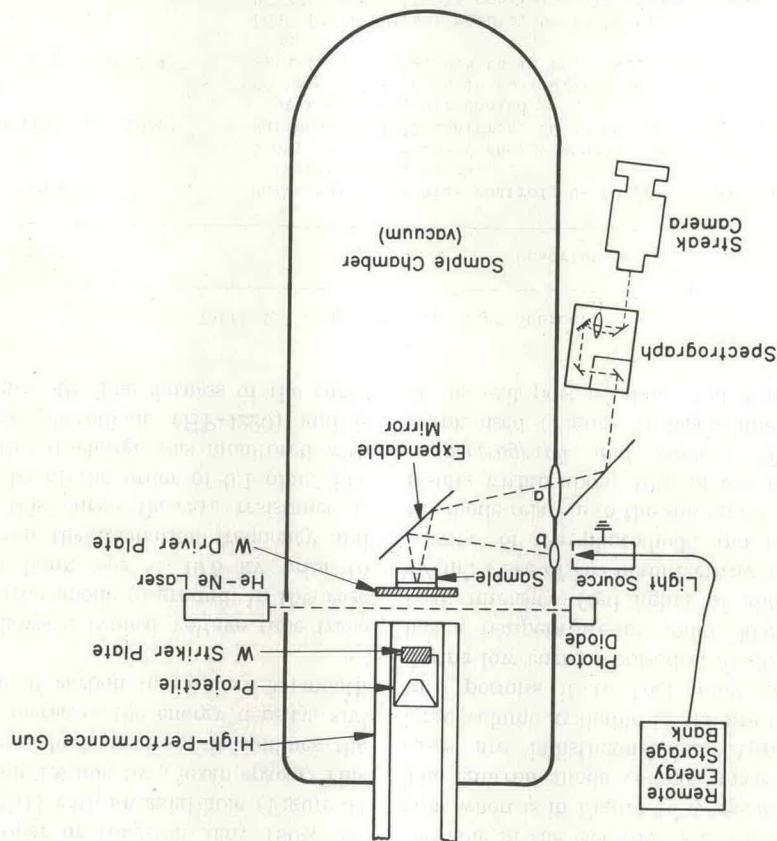


Fig. 1. Scenematic gross section of spectrographic system designed to measure optical absorption during shock loading to pressures in excess of 500 Kb. Lens  $a$  is 308 mm, lens  $b$  has a positive meniscus of 58 mm and a 7.5 diopter.



Hyer plates that produce intense shock waves in minerals upon impact. The spectrophotograph system described below, although spectrally designed for use in our system, could be adapted for use in most shock facilities, including those using high explosives. Briefly, light from a sample by an optic system and is internally reflected back along a similar path (Figure 1). The incoming and outgoing rays diverge slightly (13°) and permit the incoming rays to be focused on the entrance slit of a simple reflection grating spectrophotograph. The exit part of the spectrum is a slit, elongated in the direction of dispersion, which is the object scene for a streak camera. The resulting image is a plot of light intensity as a function of wavelength and time.

*Light source.* The light source is a confined electric discharge in air and is viewed axially

EXPERIMENTAL TECHNIQUE

For these reasons we developed a system capable of measuring optical absorption spectra of minerals while they are in a dynamically produced, high-pressure shock state. Our system is described and its present capabilities illustrated in the discussion of results for periclase shocked previously, although single-frame spectra of shocked liquids [David and Eudell, 1960] and time-resolved spectra of shocked liquids [Akusheva et al., 1971] using explosive argon light sources have been reported. The use of such explosive sources is not practicable in a shock facility such as that at Chatech, where a high-performance gun is used to accelerate a projectile of mass  $m$  to velocity  $v$ . The energy available for the compression of the sample is given by the equation

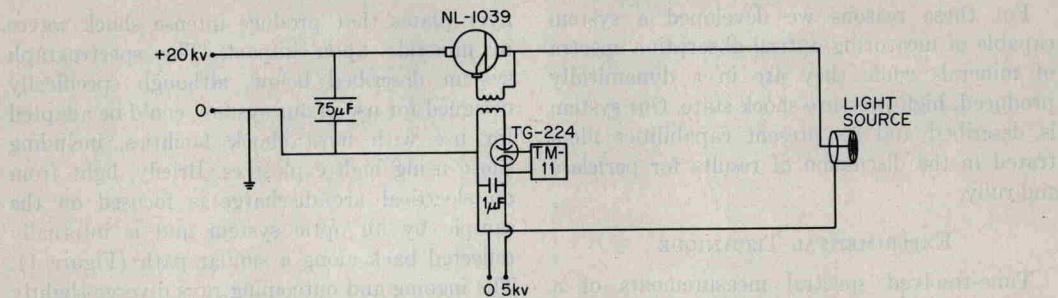


Fig. 2. Circuit diagram of a high-intensity point light source used to measure spectra in shocked solids. Components are described in Table 1.

through the ground electrode. The design is modified from that of Preonas and Swift [1970]. The electrical energy is stored at 20 kv in a 75- $\mu$ F capacitor bank (15,000 joules). The circuit is shown in Figure 2, and the components are described in Table 1. The discharge is between a central copper electrode and a ground electrode (copper or tungsten alloy (90% W, 6% Cu, 4% Ni)) with an axial hole (Figure 3) separated about 1.6 mm by a lexan spacer. This spacer serves a dual purpose; it confines the arc and thus increases the energy density, and it is a source of carbon to produce a smooth spectrum.

Figure 4 shows a typical voltage time trace from the ignitron anode to ground. In this case the capacitor bank was at 19.5 kv prior to discharge. From the oscillation frequency and damping of this curve the arc resistance is estimated to be of the order of 0.1 ohm. The intensity of this discharge was monitored with a red-sensitive photodiode (HP-4220) and is shown in Figure 4b. The flatness of the curve

between 25 and 45  $\mu$ sec is not real but is produced by saturation of the diode. The peak intensity is probably within about 10% of the value of saturation. Comparison of the curve in Figure 4d with that in Figure 4b illustrates the sensitivity of light intensity to the detailed geometry of the gap. In the case of Figure 4b, the hole in the electrode was 1.6 mm in diameter, whereas in Figure 4d it was about 3.2 mm. The ignitron anode voltage curves for the two cases are indistinguishable. Apparently, the large volume available to the arc in the second case permits it to cool much more rapidly during low current episodes. At 20 kv the light has a temperature of about 60,000°K and a peak intensity (red light) of about  $5 \times 10^8$  w/cm<sup>2</sup>. (Use of the manufacturer's 'typical sensitivity' of the photodiode and calibration of the diode relative to the sun on a clear day yield results within about 10% of one another.)

*Spectrograph and camera.* The spectrograph used (Figure 5) has a linear dispersion at the exit port of about 100 A/mm. The exit

TABLE 1. Components of Light Source

Component	Description
Power supply (main)	Universal Voltronics control, 0- to 32-kv direct current (reversible), 25 ma.
Capacitor bank	5 Aerovox 15- $\mu$ F 20-kv energy storage capacitors in parallel.
Switching ignitron (NL-1039)	National NL-1039 ignitron, 20-kv peak anode voltage, 100-ka peak current, air cooled.
Power supply (trigger)	Beckman 1150-1 0 to 10 kv (reversible), 9 ma.
Triggered spark gap (TG-224)	Signalite TG-224, 0.5 to 18 kv, 6 kilojoules, triggered spark gap.
Trigger module (TM-11)	EG&G TM-11 trigger module, 0- to 30-kv output remote trigger.
Cable	RG-221, 14-kv 50-ohm coaxial cable (armored).
Transformer	Three turns of coaxial cable (RG14/U), ignitron on center conductor.